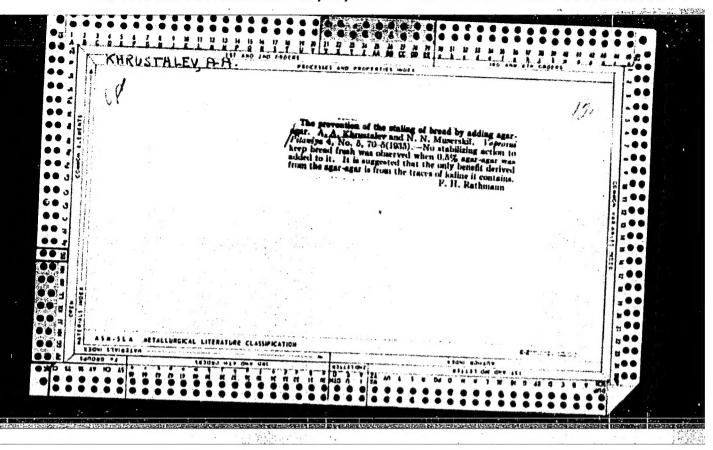
SHNEYBERG, Yakov Abramovich; ZOTIKOV, V.Ye., retsenzent; KHRUSTAL',
N.V., red.; KOVALENKO, V.L., tekhn. red.

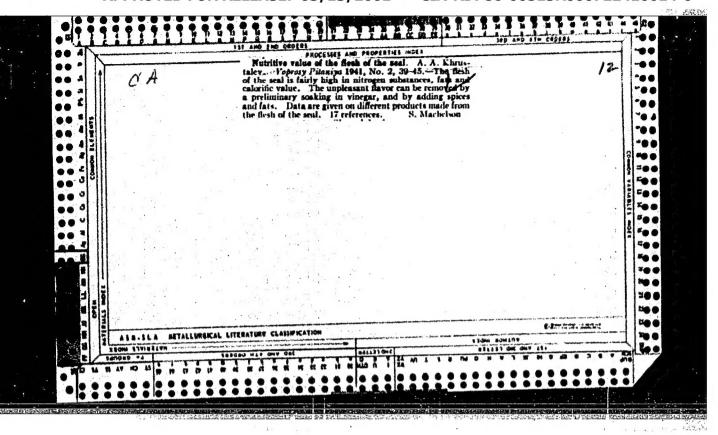
[At the sources of electrical engineering; life and work of
Academician V.V.Petrov, the first Russian electrical
engineer] U istokov elektrotekhniki; zhizn' i deiatel'nost'
pervogo russkogo elektrotekhnika akademika V.V.Petrova. Moskva, Uchpedgiz, 1963. 145 p. (MIRA 16:6)
(Petrov, Vasilii Vladimirovich, 1761-1834)
(Electric engineering)

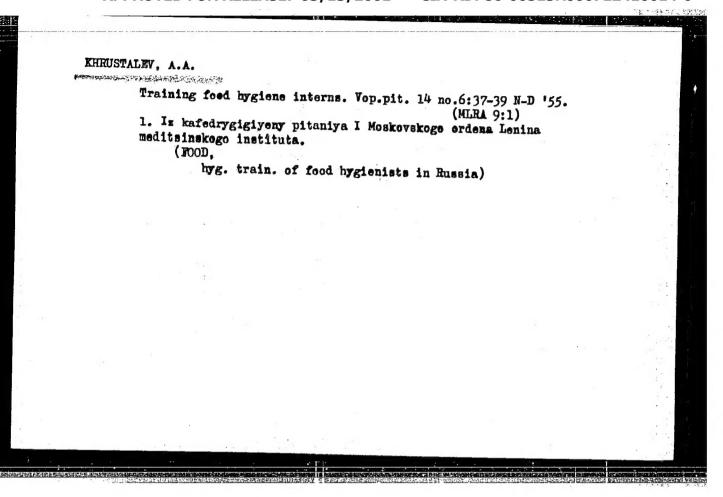
KUDRYAVTSEV, Pavel Stepanovich; KONFEDERATOV, Ivan Yakovlevich; KHRUSTAL', N.V., red.

[History of physics and technology; manual for students of pedagogical institutes] Istoriia fiziki i tekhniki; uchebnoe posobie dlia studentov pedagogicheskikh institutov. Izd.2., perer. i dop. Moskva, Prosveshchenie, 1965. 570 p. (MIRA 18:7)

Precast reinforced concrete floors for multistory industrial buildings in Hungary. Biul. stroi. tekh. 14 no.2:36-39 F '56. (MIRA 10:4) (Hungary-Precast concrete construction) (Floors, Concrete)







KHRUSTALEV, A.A., predsedatel' sektsii pitaniya; SHARINA, Ye.G., sekretar'

Work of the nutrition section of the Moscow branch of the All-Union Hygiene Society in 1955. Vop.pit. 15 no.4:63 Jl-Ag '56. (MIRA 9:9) (NUTRITION)

Experiments and hygiene research in the work of F. F. Brisman on nutrictional hygiene. J. Hyg. Epidem., Praha 1 no.4:504-511 1957,

1. Ghair of Mutritional Eygiene, Sechenov Medical Institute, Moscow.
(NUTRIFICM,
hyg., contribution of F. F. Brisman)
(BIOGRAPHIES,
Brisman, F.F.)

KHRUSTALEV, A.A., professor; ALEKSANDROVA, N.N., assistant kafedry

List of dissertations on nutritional hygiene and associated problems defended from January, 1822 to May, 1956. Vop.pit. 16 no.3:81-96 My-Je 157. (MLRA 10:10)

1. Zaveduyushchiy kafedroy gigiyeny pitaniya I Moskovskogo ordena Lenina meditsinskogo instituta imeni I.M.Sechenova (for Khrustalev) (NUTRITION, bibliog. (Rus))

KHRUSTALEV, A.A., professor; SHARIMA, Ye.G.

Work of the nutrition section of the Moscow Branch of the All-Union Hygiene "ociety during 1956. Vop.oit. 16 no.4:90-91 J1-Ag 157. (MLHA 10:10)

1. Predsedatel' sektsii pitaniya Moskovskogo otdeleniya Vsesoyuznogo gigiyenicheskogo obshchestva (for Khrustalev). 2. Sekretar' sektsii pitaniya Moskovskogo otdeleniya Vsesoyuznogo gigiyenicheskogo obshchestva (for Sharina) (NUTRITION)

# KHRUSTALEV. A.A., prof.

Hygienic principles for planning a kitchen block. Gig. i san. 22 no.9:82-85 \$ '57. (MIRA 10:12)

Iz kafedry gigiyeny pitaniya I Moskovskogo ordena Lenina meditainskogo inatituta imeni I.M.Sechenova.
 (HOSPITAL ADMINISTRATION

hygienic principles of isolated kitchen block)

KHRUSTALEV, A. A.

"Rationalization of nutrition of agricultural workers."

report submitted at the 13th All-Union Congress of Hygienists, Epidemologists and Infectionists, 1959.

KHRUSTALEV, A.A.; ALEKSANDROVA, N.N.; GIAZATOVA, A.F.

Feeding of miners in the mines. Vop. pit. 19 no.3:15-17 My-Je 160. (MIRA 14:3)

1. Iz kafedry gigiyeny pitaniya (zav. - prof. A.A.Khrustalev) I Moskovskogo ordena Lenina meditsinskogo instituta imeni I.M. Sechenova i sanitarno-epidemiologicheskoy stantsii Shchekinskogo rayona Tul'skoy oblasti.

(COAL MINERS DISEASES AND HYGIENE) (NUTRITION)

# KHRUSTALEV, A.A.

Exercise therapy in operations on the lungs. Vop. kur., fizioter. i lech. fiz. kul't. 26 no.6:544-547 N-D '61. (MIRA 15:1)

1. Iz kafedry lechebnoy fizcheskoy kul'tury (zav. - prof. V.N.Moshkov)
TSentral'nogo instituta usovershenstvovaniya vrachey.
(EXERCISE THERAPY) (LUNGS\_\_THERAPY)

MIKHIREV, P.A.; SINYUGIN, G.M.; KHRUSTALEV, A.A.

MPDR-0.12 loading and hauling machine. Gor. zhur. no.9:54-55 S '62. (MIRA 15:9)

1. Institut gornogo dela Sibirskogo otdeleniya AN SSSR (for Mikhirev). 2. Rudnik "Emel'dzhak" kombinata Aldanslyuda (for Sinyugin). 3. Gosudarstvennyy institut po proyektirovaniyu predpriyatiy nikelevoy promyshlennosti (for Khrustalev).

(Mining machinery)

TUPOLEV, M.S., doktor arkh. prof.; POPOV, A.N., prof.; POPOV, A.A., kand. arkh. dots.; SHKINEV, A.N., inzh., dots.; KHRUSTALEV, A.A., kand. arkh. dots.; NEYSHTADT, L.I., nauchnyy red.; FEDOROVA, T.N., red. izd-va; KOROBKOVA, N.I., tekhn. red.

[Public and industrial buildings] Grazhdanskie i promyshlennye zdaniia. Pod obshchei red.M.S.Tupoleva. Moskva, Gosstroiizdat. Pt.2.[Industrial buildings] Promyshlennye zdaniia. 1963. 198 p. (MIRA 16:7)

1. Chlen-korrespondent Akademii stroitel'stva i arkhitektury SSSR (for Popov, A.N.). 2. Prepodavateli Moskovskogo arkhitekturnogo instituta (for Tupolev, Popov, A.N., Popov, A.A., Shkiney, Khrustalev).

(Industrial buildings)

KHRUSTALEV, A.A. (Moskva)

Medical gumnastics for patients suffering from lung diseases and treated by surgery. Med. sestra 22 nd.10:32-36 0'63 (MIRA 16:12)

1. Iz kafedry lechebnoy fizkul'tury TSentral'nogo instituta usovershenstvovaniya vrachey.

KHRUSTALEV, A.A., kand. med. nauk

Effect of exercise therapy on the function of external respiration following lung surgery. Trudy TSIU 66:168-175 '64. (MIRA 18:5)

AMRUSTALEV, A.A., inzh.

Logical synthesis of a three-phase automatic reclosing device. Tzv.vys.ucheb.zav.; energ. 8 no.10:16-23 0 465.

(MIRA 18:10)

1. Moskovskiy ordena Lenina energeticheskiy institut. Predstavlena kafedrov elektricheskikh stantsiy.

KHRUSTALEV, A. F.: Master Phys-Math Sci (diss) -- "A solution of some axialsymmetric problems in the theory of elasticity with mixed boundary conditions".

Moscow, 1958. 5 pp (Min Higher Educ USSR, Moscow Order of Lenin and Order of
Labor Red Banner State U im M. V. Lomonosov), 150 copies (KL, No 6, 1959, 125)

AUTHOR:

Khrustalev, A.F. and Kogan B.I.

SOV/140-58-3-31/34

TITLE:

On a Boundary Value Problem for the Biharmonic Equation Occurring in Elasticity Theory (Ob odnoy granichnoy zadache dlya bigarmonicheskogo uravneniya, vstrechayushcheysya v teorii uprugosti)

PERIODICAL: Izvestiya vysshikh uchebnykh zavedeniy Matematika, 1958, Nr 3, pp 241-247 (USSR)

ABSTRACT:

The authors consider the solution of such axialsymmetric elasticity problems for the infinite circular cylinder which lead to the determination of the stress function  $\chi(r,z)$  which in the cylindrical coordinate system satisfies the biharmonic

equation  $\nabla^4 \chi(\mathbf{r}, \mathbf{z}) = 0$  and the boundary conditions

$$\sigma_{r} = \frac{\partial}{\partial z}(y \nabla^{2} \chi - \frac{\partial^{2} \chi}{\partial r^{2}}) = 0$$
 for r=R,  $0 < z < \infty$ 

$$v_{rz} = \frac{\partial}{\partial r} \left[ (1-y) \nabla^2 \chi - \frac{\partial^2 \chi}{\partial z^2} \right] = 0$$
 for  $r = \omega$ ,  $-\infty < z < \infty$ 

Card 1/2

On a Boundary Value Problem for the Biharmonic Equation Occurring in Elasticity Theory

SOV/140-58-3-31/34

 $d\sigma_r + \beta u = y$  for r=R,  $-\infty < z < 0$ ,

where  $u = -\frac{1+y}{E} \frac{\partial^2 \chi}{\partial r \partial z}$ ,  $\alpha \downarrow >0$ ,  $\beta >0$ .

The solution is obtained by skillful combination of the methods of one of the authors [Ref 2] and of Al'perin [Ref 1]. There are 2 Soviet references.

ASSOCIATION: Khar'kovskiy avtomobil'no-dorozhnyy institut (Kharkov Highway Institute)

SUBMITTED: November 23, 1957

Card 2/2

KOG/N, B.I.; KHRUSTALEV, A.F. (Khar'kov)

Axisymmetric problem of the elasticity theory for a hollow cylinder.
Prikl.mat. 1 mekh. 22 no.5:683-686 S-0'58. (MIRA 11:11)

(Elasticity)

16(1) AUTHORS:

Khrustalev, A.F., Kogan, B.I.

SOV/140-59-4-22/26

TITLE:

On the State of Stress of a Hollow Circular Cylinder

PERIODICAL:

Izvestiya vysshik uchebnykh zavedeniy. Matematika, 1959,

Nr 4 pp 178 - 183 (USSR)

ABSTRACT:

The authors consider axial symmetric problems of elasticity theory of the infinite hollow circular cylinder which lead to the determination of the stress function  $\gamma(r,z)$  from the

biharmonic equation  $\nabla^4 \varphi(r,z) = 0$  and from the boundary

conditions

 $r = r_2$ ,  $- \infty < z < \infty$ ;  $r = r_1$ ,  $0 < z < \infty$ 6° = 0

 $t'_{rz} = 0$  for  $r = r_1$ ,  $r = r_2$ ,  $-\infty < z < \infty$ 

 $6 + 8u = \gamma$  for  $r = r_1$ ,  $-\infty < z < 0$ 

The solution is obtained by function-theoretical auxiliary means according to the scheme of [ Ref 1,2].

Card 1/2

On the State of Stress of a Hollow Circular Cylinder

SOV/140-59-4-22/26

The authors give three special cases (special values of  $\ll$ 

There are 2 Soviet references.

ASSOCIATION: Khar'kovskiy avtomobil'no-dorozhnyy institut (Khar'kov

Automobile Roads Institute)

SUBMITTED: May 23, 1958

Card 2/2

KOGAN, B.I. (Khar'kov); KHRUSTALEV, A.F. (Khar'kov)

Stresses caused by pressing a semi-infinite thin shell on a cylinder.

IZV.AN SSSR. Otd.tekh.nauk.Mekh.i mashinostr. no.5:176-177 8-0 '60.

(Klastic plates and shells)

(Klastic plates and shells)

Distributtion of temperature in a continuous infinite cylinder.

Izv. vys. ucheb. zav. mat. no. 6:239-243 '60. (HIRA 14:1)

1. Khar'kovskiy avtomobil'no-dorozhnyy institut.
(Mathematical physics)

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S/140/60/000/006/018/018 C111/C222

AUTHORS:

Khruatalev. A.F. and Kogan, B.I.

TITLE: On the Distribution of Temperature in a Massive Infinite Cylinder

PERIODICAL: Izvestiya vysshikh uchebnykh zavedeniy. Matematika, 1960, No. 6, pp. 239 - 243

TEXT: Let one half of a massive infinite cylinder be in a medium of constant temperature, while the other half radiates the heat into the surrounding space according to Newton's law. The problem consists in the determination of a function T(r,z) which satisfies the harmonic equation in cylindrical coordinates:



(1)  $\nabla^2 T(r, z) = 0$ 

and the boundary conditions

(2) 
$$T = T_1$$
 for  $r = R_1 - \infty < z < 0$ 

(3) 
$$\frac{\partial T}{\partial r} + hT = 0$$
 for  $r = R$ ,  $0 < z < + \infty$ ,

Card 1/4

S/140/60/000/006/018/018 C111/C222

On the Distribution of Temperature in a Massive Infinite Cylinder

where h is the coefficient of heat exchange. The author's solution is

(16) 
$$T(\varsigma,\lambda) = -\frac{hT_1}{2\pi i} \int_{-i\infty}^{o-s+i\infty} \frac{RJ_o(\varsigma u)II(u)}{u[hRJ_o(u)-uJ_1(u)]} e^{\lambda u_{du}}$$

where
$$(11) II(u) = \int_{u}^{\infty} \frac{\left(1 - \frac{u}{a}\right)}{1\left(1 - \frac{u}{b_n}\right)}$$

and an are the positive roots of the equation

(12) 
$$hRJ_{0}(u) - uJ_{1}(u) = 0$$

and  $b_n$  are the positive roots of the equation

(13) 
$$J_0(u) = 0 ,$$

$$\lambda = \frac{z}{R} , \quad S = \frac{r}{R} .$$

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S/140/60/000/006/018/018 C111/C222

On the Distribution of Temperature in a Massive Infinite Cylinder

It is stated that

For small  $\lambda > 0$  and g = 1 it holds

$$T = T_1 + \frac{T_1}{2 \pi i} \int_C \frac{e^{-V}}{V \prod \left(\frac{V}{\lambda}\right)} dV$$

where C consists of the imaginary axis, where the interval (- a, a) of it is replaced by a semicircle of radius a. For the density of the heat flow for small  $\lambda > 0$  and g = 1 the authors obtain :

$$q \sim kh T_1 \left(1 - \frac{2\sqrt{\lambda hR}}{\sqrt{\pi}}\right)$$

Card 3/4

S/140/60/000/006/018/018 C111/C222

On the Distribution of Temperature in a Massive Infinite Cylinder

The authors mention A.M. Danilevskiy. There is 1 figure and 1 Soviet reference.

ASSOCIATION: Khar'kovskiy avtomobil'no-dorozhnyy institut

(Khar'kov Automobile and Highway Institute)

SUBMITTED: November 25, 1958

. Card 4/4

KHRUSTALEV, A. F., and KOGAN, B. I.,

"Temperature Distribution in an Infinite Hollow Cylinder."

Report submitted for the Conference on Heat and Mass Transfer, Minsk, BSSR, June 1961.

24.4200 1103 1327

5/140/61/000/004/011/013

C111/C222

AUTHORS:

Khrustalev, A. F., and Vaynshteyn, F. A.

TITLE:

On a boundary value problem for the bending equation of

a thin plate

PERIODICAL:

Izvestiya vysshikh uchebnykh zavedeniy. Matematika,

no. 4, 1961, 119-124

TEXT: The authors consider a thin infinite plate of constant width b under the influence of the vertical load q(y/b). They seek the solution of the bending equation

$$\nabla^{4} w = \frac{q \left(\frac{y}{b}\right)}{D} \tag{6}$$

which satisfies the mixed boundary conditions

for y=0, 
$$-\infty < x < +\infty$$
, (1)

$$-\alpha_1 \frac{\partial w}{\partial y} = \beta_1 M(w)$$

for 
$$y = 0$$
,  $-\infty < x < +\infty$ , (2)

$$W = 0$$
 Card  $1/5$ 

for 
$$y = b$$
,  $-\infty < x < +\infty$ , (3)

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S/140/61/000/004/011/013
On a boundary value problem for the ... C111/C222
$$M(W) = -D\left(\frac{3^2W}{3x^2} + V\frac{3^2W}{3x^2}\right) = M_0 \quad \text{for } y = b, -\infty < x < 0, \quad (4)$$

$$\alpha_2 \frac{\partial W}{\partial y} = \beta_2 M(W) \qquad \text{for } y = b, \ 0 < x < +\infty. \ (5)$$

The arrangement

$$W = \varphi(y) + W_1 \tag{7}$$

is made, where it shall be

$$\nabla^{4}\mathbf{w}_{1} = 0 \tag{8}$$

and it is stated that the solution has the form

Card 2/5

32738 5/140/61/000/004/011/013On a boundary value problem for the ... C111/C222  $W = \frac{1}{D} \left[ \frac{b^4}{6} \int_{0}^{\xi} (\xi - \hat{\xi})^3 q(\xi) d\xi + Ab^3 \xi^3 + Bb^2 \xi^2 + Cb \xi \right] + \frac{M_1}{2\pi iD} \int_{-i\infty}^{b^2} \frac{\prod_{i=1}^{d} (u)}{u^2} \frac{\Psi_0(u)}{\Psi(u)} e^{\lambda u} du$   $\text{where } \xi = \frac{\chi}{b},$   $B = \frac{b^2 a_i \int_{0}^{1} (1 - \xi) [2D_{i,2}^3 + ba_2(1 - \xi) - (ba_2 + 2D_{i,3})(1 - \xi)] q(\xi) d\xi}{2(\epsilon^2 a_1 a_2 + 4Dba_1 \beta_2 + 4Dba_2 \beta_3 + 12D^2 \beta_1 \beta_3)},$   $C = \frac{2D\beta_1}{a_1} B,$   $A = -\frac{b}{6} \int_{0}^{1} (1 - \xi)^2 q(\xi) d\xi - \frac{B}{b} - \frac{C}{b^3}.$  Card 3/5

 $M_{1}=M_{0}+b^{2}\int_{0}^{1}(1-\xi)q(\xi)d\xi+6Ab+2B, \int_{0}^{2}\frac{b^{2}\alpha_{1}\alpha_{2}+4bD(\alpha_{1}\beta_{2}+\alpha_{2}\beta_{1})+12D^{2}\beta_{1}\beta_{2}}{4b\alpha_{1}+12D\beta_{1}}$   $\prod_{n=1}^{\infty}(u)=\prod_{n=1}^{\infty}\frac{\left(1-\frac{u}{a_{n}}\right)}{\left(1-\frac{u}{b_{n}}\right)},$ On a boundary value problem for the ...

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are the roots of the equation  $\psi(u) = 0$  in the right halfplane, are the roots of the equation  $\Psi(u) = 0$  in the right halfplane,

$$mb = u, \ x = \lambda b, \ B_1(u) = K(u) \frac{a_1(u \cos u - \sin u)}{u\psi(u)},$$

$$\varphi(u) = u \left(2ba_1u + 4D\beta_1u \sin^2 u - ba_1\sin 2u\right),$$

$$\psi(u) = \left[b^2a_1a_2 + 2Db\left(a_1\beta_2 + a_2\beta_1\right)\right]u^2 + \left(4D^2\beta_1\beta_2u^2 - b^2a_1a_2\right)\sin^2 u - Db\left(a_1\beta_2 + a_2\beta_1\right)u \sin 2u.$$

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\$\frac{5}{140}/61/000/004/011/013\$

On a boundary value problem for the ... \$\frac{C111}{C222}\$

\$\psi\_0(u) = \text{box}(u \cos u - \sin u) \mathbb{g} u \sin \mathbb{g} u + (2D\beta\_1 u \cos u + \text{box} \sin u),

and \$\lambda = \frac{x}{b}\$.

Explicit expressions for \$\lim\_{\text{W}} \text{W}, M(\text{W}) \sqrt{\lambda} \rightarrow 0(\lambda > 0)

and \$\frac{3}{4} \text{W} \sqrt{\lambda} \rightarrow 0(\lambda > 0)

and further similar ones are given.

\$\frac{2}{4} \text{W} \rightarrow 0(\lambda > 0)

\$\frac{2}{4} \text{V} \rightar

Card 5/5

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AUTHOR:

Khrustalev, A. F.

TITLE:

Temperature field in an unbounded plane wall

PERIODICAL: Inzhenerno-fizicheskiy zhurnal, v. 4, no. 11, 1961, 81-88

TEXT: The author studies the steady temperature field of an unbounded plane wall. The heat-exchange coefficient between the heat-supplying medium (constant temperature) and the wall (thickness 2b) is  $h_0$ . h is the heat-exchange coefficient between the wall and the heat-absorbing medium (temperature  $0^{\circ}$ C). The heat distribution T(x,y) to be found satisfies the Laplace equation  $\frac{\partial^2 T}{\partial x^2} + \frac{\partial^2 T}{\partial y^2} = 0$  and the boundary conditions  $\frac{\partial T}{\partial x} + \frac{\partial T}{$ 

Card 1/4

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Temperature field in an ...

$$T(\rho;\lambda) = -\frac{hb}{2\pi i} \int_{-\infty}^{0-i+l} \frac{\Pi(u)}{u} \frac{\cos\rho u}{bh\cos u - u\sin u} e^{\lambda u} du = \frac{hb}{\pi} \int_{0}^{\infty} \frac{\operatorname{Im}\left[\Pi\left(iz\right)e^{i\lambda z}\right]}{z} \frac{\operatorname{ch}\rho z}{bh\operatorname{ch}z + z\operatorname{sh}z} dz + \frac{T_{0}}{2}$$

$$(16)_{n}$$

where  $x = Qb, b, y = \lambda b, u = mb$ ,

 $\Pi(u) = \prod_{k=1}^{\infty} \frac{1-u/a_k}{1-u/b_k}$  are positive roots of the equation bh cos u

-ucos u = 0, and  $b_k$  are positive roots of the equation  $b_0\cos u - u\sin u=0$ . This solution is discussed. It is shown that the temperature at  $\varrho=\pm 1$  and  $\lambda=0$  is a continuous function when its derivative with respect to  $\varrho$  and the heat-flow density have discontinuities at this point. Finally,  $T(\varrho,\lambda)$  is derived for  $h\longrightarrow h_0$ :

Card. 2/4

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#### "APPROVED FOR RELEASE: 03/13/2001

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Temperature field in an ... B104/B112  $T(\rho;\lambda) = -\frac{bT_{\bullet}(\alpha + \beta h + \alpha hb)}{2\pi i (\beta + \alpha b)} \int_{-i}^{-i+1} \frac{\Pi(u)(u\beta \cos \mu u + \alpha b \sin \mu u)e^{iu}du}{u[ub(\alpha + \beta h)\cos u + (h\alpha b^3 - u^3\beta)\sin u]}$   $= \frac{bT_{\bullet}(\alpha + \beta h + \alpha hb)}{\pi(\beta + \alpha b)} \int_{-i}^{i} \frac{Im[\Pi(ix)e^{i\lambda x}](z\beta \cosh \rho z + \alpha b \sinh \rho z)dz}{z[zb(\alpha + \beta h) \cosh z + (h\alpha b^3 + z^3\beta) \sinh z]} + \frac{(\beta + \alpha b)T_{\bullet}}{2(\beta + \alpha b)}$ This solution satisfies the boundary conditions  $aT - \beta \frac{\partial T}{\partial x} = 0 \quad \text{nph } x = 0, \quad -\infty < y < +, \infty; \quad (24-(26)),$   $\frac{\partial T}{\partial x} + MT = 0 \quad \text{nph } x = b, \quad 0 < b < +, \infty;$ 

Temperatu	re field in		28909 s/170/61 B104/B11	25909 s/170/61/004/011/009/020 B104/B112			
	$T = T_0$	to the second	$-b, -\infty < y < 0,$	<del>। । । । । । । । । । । । । । । । । । । </del>			
where a a	nd β are non references.	-negative paramet	ers. There are	2 figures and	:		
SUBMITTEL	), April 8,	1961		•	W		
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26.5100

AUTHOR:

Khrustalev, A. F.

Heat transfer through a cylinder wall

PERIODICAL: Inzhenerno-fizicheskiy zhurnal, v. 4, no. 12, 1961, 98 - 101

The steady temperature field of a hollow cylinder of infinite length was examined under the boundary conditions (1)

 $\alpha T - \beta \frac{\partial T}{\partial r} = 0 \text{ nph } r = r_1, -\infty < z < \infty,$ 

 $\frac{\partial T}{\partial r} + hT = 0 \text{ nph } r = r_2, 0 < z < +\infty.$   $\frac{\partial T}{\partial r} + h_0 T = h_0 T_0 \text{ nph } r = r_2, -\infty < z < 0,$   $h_0 = \text{heat-transfer coefficient between the heat-emitting medium and the}$ cylinder wall; h = heat-transfer coefficient between cylinder wall and heat-absorbing medium; r<sub>1</sub> and r<sub>2</sub> = external and the internal radii of the Card 1/4

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Heat transfer through a cylinder ...

B is then regarded as a function of the parameter m, and the integral

$$T(r; z) = \int_{-\infty}^{\infty -i} T_1(r; z; m) dm, \qquad (9)$$

is set up. On the basis of the foregoing and after extensive calculations

the exact solution

 $T(\rho, \lambda) = -h_0 T_0 r_2 (\alpha n + \beta h - \alpha n h r_2 \ln n) \int_{-\infty}^{\alpha - \frac{1}{2} + 1 - \alpha} \Pi(u) u^{-1} \times$ (18)

 $\times \varphi(\rho, u)e^{\lambda u} du [2\pi i (\alpha n + \beta h_0 - \alpha n h_0 r_1 \ln n]^{-1} = -h_0 T_0 r_1 (\alpha n + \beta h - \alpha n h_0 r_2 \ln n)^{-1}$ 

 $= \alpha \, nhr_1 \ln n) \left[ \pi \, (\alpha \, n + \beta \, h_0 - \alpha \, nh_0 r_1 \ln n) \right]^{-1} \int_0^\infty Im \left[ \Pi \, (iy) \, e^{i \, \lambda \, y} y^{-1} \, \phi \, (\rho; iy) \, dy + \frac{1}{2} \left[ \frac{1}{2}$ 

 $\begin{array}{ll}
\text{Willief?} & +h_0T_0[n\,\alpha\,r_2\,(\ln\rho-\ln n)+\beta]\,[2\,(\,\alpha\,n+\beta\,h_0-\alpha\,nh_0r_2\,\ln n)]^{-1},\,(18) \\
\varphi(\rho;\,u) & = \varphi_1^{-1}(u)\,[\alpha\,r_2I_0(nu)+\beta\,uI_1(nu)]\,H_0^{(1)}(\rho\,u)-[\alpha\,r_2H_0^{(1)}(nu)-1]
\end{array}$ 

 $\beta uH(^{(1)}(nu))I_0(\rho u). \tag{19}$ 

Card 3/4

is obtained. Here,  $u = mr_2$ ,  $r = r_2$ , and  $z = r_2$ . There are 2 Soviet references.

SUBMITTED: April 3, 1961

Card 4/4

\*1,000,000

S/020/61/141/002/008/027 B104/B138

211000 AUTHOR:

Khrustalev, A. F.

TITLE:

A boundary value problem of the Laplace equation

PERIODICAL: Akademiya nauk SSSR. Doklady, v. 141, no. 2, 1961, 327-329

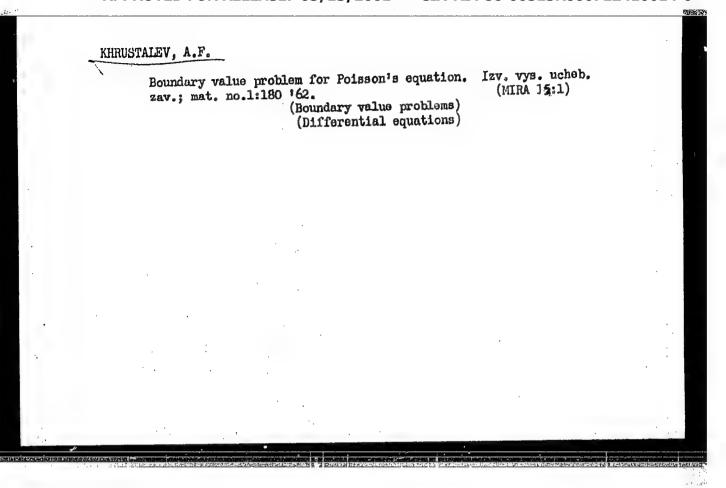
TEXT: The paper deals with a method for the determination of the steady temperature field of an unbounded hollow cylinder whose inner surface is coated with thermal insulation and whose outer surface exhibits the temperature T = f(z) on half its length, while the second half emits heat according to Newton's law. The solution of the problem in question must satisfy the Laplace equation at the boundary conditions  $\partial T/\partial r = 0$  ( $r = r_1$ ,  $-\infty < z < +\infty$ ),  $\partial T/\partial r + hT = 0$  ( $r = r_2$ ,  $0 < z < +\infty$ ) and T = f(z) ( $r = r_2$ ,  $-\infty < z < 0$ ). f(z) can be, and is here, represented as a Fourier integral. The condition  $T = A\cos\beta z = \frac{A}{2}$  ( $e^{i\beta z} + e^{-i\beta z}$ ) is chosen for T, for  $r = r_2$ ,  $-\infty < z < 0$ , where A and  $\beta$  are real parameters. The solution of the problem discussed is found from Card 1/2

N

A boundary value problem of the...  $\frac{S/020/61/141/002/008/027}{B104/B138}$   $T_{1}(\rho,\lambda) = \int_{\Gamma} \frac{[H_{0}^{(i)}(\rho u)J_{1}(nu) - J_{0}(\rho u)H_{0}^{(i)}(nu)]k(v)}{\varphi_{1}(u)} e^{\lambda u} du = A\varphi(\rho,\lambda,\beta), \quad (13)$ where  $\varphi(\rho,\lambda,\beta) = -\frac{1}{2\pi} \int_{\varphi_{1}([\rho x])}^{0} \frac{[\varphi_{1}([\rho x])] \operatorname{Im} \left\{ \frac{1}{|\Pi(-ix)|} \left[ \frac{\Pi(-ix)}{x - \beta r_{0}} + \frac{\Pi([\beta r_{0})}{u + \beta r_{0}} \right] e^{i\lambda x} \right\} - \frac{\varphi_{1}([\beta r_{0})}{\varphi_{1}([\beta r_{0})](x - \beta r_{0}} + \frac{1}{x + \beta r_{0}}) \sin \lambda x} \right] dx + \frac{\varphi_{1}([\beta \beta r_{0})}{\varphi_{2}([\beta r_{0})} \cos \lambda \beta r_{0};$   $\varphi_{2}([ipx) = H_{0}^{(i)}([ipx)J_{1}([inx) - J_{0}([ipx)H_{0}^{(i)}([inx)] = \frac{2}{\pi} |k_{0}(\rho x)I_{1}(nx) - K_{1}(nx)I_{0}(\rho x)|,$ Here  $x = \xi x_{2}$ ,  $x = \lambda x_{2}$ . There are 2 Soviet references.

PRESENTED: July 17, 1961, by S. L. Sobolev, Academician

SUBMITTED; July 8, 1961



37611 s/143/62/000/004/005/006 D238/D307

26.5100

AUTHOR:

Khrustalev, A.F., Candidate of Physico-Mathematical

Sciences

The temperature field of an infinite solid cylinder

Izvestiya vysshikh uchebnykh zavedeniy. Energetika, 196.5 TITLE:

PERIODICAL: no. 4, 1962, 104 - 107

TEXT: For the purpose of studying the steady-state temperature field of an infinite solid cylinder with radius R, within which heat sources are distributed with a density depending only on the radius, it is assumed that the cylinder is charged to one half of its length with a heat-generating medium at a constant temperature To and the other half delivering the heat to a heat-absorbing medium the temperature of which is zero. It is assumed that the heat exchange bet-ween the end surfaces of the cylinder and the surrounding medium follows Newton's law. Calling the coefficient of heat exchange between the heat-transmitting medium and the cylinder ho and the coefficient of heat exchange between the cylinder and the heat-absorbing medium h, the function of temperature distribution corresponding to these Card 1/3

S/143/62/000/004/005/006 D238/D307

The temperature field of an ...

requirements takes on the form of a solution of the Poisson equation in the cylindrical system of coordinates:

$$\Delta T = \frac{\partial^2 T}{\partial r^2} + \frac{1}{r} \cdot \frac{\partial T}{\partial r} + \frac{\partial^2 T}{\partial z^2} = -\frac{Q(\frac{r}{R})}{k}$$
 (1)

satisfying the boundary conditions:

$$\frac{\partial T}{\partial r} + hT = 0 \qquad \text{for } r = R; \ 0 < z < + \omega, \tag{2}$$

$$\frac{\partial T}{\partial r} + h_0 T = h_0 T_0 \quad \text{for } r = R - \omega < z < 0.$$
 (3)

To solve (1) it is brought to a homogeneous form assuming

$$T = \varphi(\frac{r}{R}) + T_1 \tag{4}$$

Frequiring that  $\triangle T_1 = 0$  (5). From (4) and (5), taking into account the boundedness of the solution at the axis of the cylinder, it follows that Card 2/3

395h3 5/170/62/005/008/008/009 B104/B102

26.5100

AUTHOR:

Khrustalev, A. F.

TITLE:

Heat conduction of a solid cylinder

PERIODICAL:

Inzhenerno-fizicheskiy zhurnal, v. 5, no. 8, 1962, 101-105

TEXT: The stationary temperature field of an unbounded solid cylinder is studied under the boundary conditions

$$T=0$$
 npH  $r=R$ ,  $|z| \gtrsim a$ ;

 $\frac{\partial T}{\partial r} + hT - hf(z) \quad \text{при} \quad r = R, \ |z| < a.$ 

(2),

where h is the heat exchange coefficient between cylinder and surrounding medium and f(z) is an even function describing the temperature of that medium. The formulation

 $T(r;z) = \int_{0}^{\infty} A(m)I_{0}(mr) \cos mz \, dm$  satisfies the Laplace equation in

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cylinder is stud T = 0; half the conditions heat in is reduced to the	nto the surre	ounding medium of harmonic equitions. The mey solution of the	m accordinations in athod of some form	ing to Newton cylindrical olving these	n's law.	tes with is pre	n cor- esented

L 13067-63 EMP(r)/EMP(q)/EMT(m)/EDS AFFTC/ASD JD
ACCESSION NR: AP3000957 S/0140/63/000/003/0162/0165

AUTHOR: Khrustalev, A. F. (Khar'kov); Vaynshteyn, F. A. (Khar'kov)

TITLE: A mixed problem in elasticity theory for transverse isotropic hollow cylinder

SOURCE: IVUZ. Matematika, no. 3, 1963, 162-165

TOPIC TAGS: elasticity, isotropic cylinder, partial differential equation

ABSTRACT: The author considers a mixed problem in elasticity theory for a transverse isotropic hollow circular cylinder which reduces to the determination of the stress function X(r,z) satisfying the system in the Enclosure. The problem is solved. Orig. art. has: 23 formulas.

ASSOCIATION: none

SUBMITTED: 22Feb60 DATE ACQ: 12Jun63 ENCL: 01

SUB CODE: OO NO REF SOV: COS CTIER: CO

Card 1/2/

Mixed problem in the theory of elasticity for a layer. Insh. shur. 3 no.2:391-393 '63. (MIRA 16:6)

(Elasticity)

KHRUSTALEV, A.F. (Khar'kov)

Boundary value problem for Poisson's equátion, 12v. vys. ucheb.

zav.; mat. no.5:129-132 '63. (MIRA 16:11)

45118

B102/B186

8/170/63/006/002/011/01

265100

AUTHOR:

Khrustalev, A. F.

TITLE:

The thermal conductivity of an infinite plane wall

PERIODICAL: Inzhenerno-fizicheskiy zhurnal, v. 6, no. 2, 1963, 82 - 87

TEXT: Consideration is given to a plane wall of infinite extent, one half of which is surrounded by a heat giving and the other half by a heat-absorbing medium. The temperature of the heat removing medium changes only in the axial direction  $T_1 = f(x)$ . The problem is to find the function T(x,y,z) which has to satisfy the Laplace's equations and certain boundary conditions. If these latter are given by

$$\pm \frac{\partial T}{\partial y} + hT = 0 \qquad \text{прн } y = \pm b, |x| < \infty, 0 < z < +\infty; \tag{2},$$

$$\pm \frac{\partial T}{\partial y} + h_0 T = h_0 f(x) \quad \text{при } y = \pm b, |x| < \infty, -\infty < z < 0.$$
 (3)

Card 1/3

The thermal conductivity of an...

S/170/63/006/002/011/018 B102/B186

one obtains

$$T = -\frac{bh_0}{2\pi i} \int_{-\infty}^{+\infty} a(\beta) A(\beta) \cos \beta x d\beta \times .$$

$$\times \int_{-l\infty}^{0-1+l\infty} \frac{\Pi(u,\beta)\cos(\sqrt{u^2-b^2\beta^2})\rho\exp(uv)\,du}{u\,(hb\cos\sqrt{u^2-\beta^2b^2}-\sqrt{u^2-\beta^2b^2}\sin\sqrt{u^2+\beta^2b^2})}$$
(14)

If they are given by

$$\alpha T - \lambda \frac{\partial T}{\partial y} = 0 \quad \text{при } y = 0, \quad |x| < \infty, \quad |z| < \infty; \tag{15}$$

$$\frac{\partial I}{\partial y} + hT = 0 \quad \text{при } y = b, |x| < \infty, \ 0 < z < +\infty; \tag{16}$$

$$\frac{\partial T}{\partial y} + h_0 T = h_0 f(x) \text{ при } y = b, |x| < \infty, -\infty < z < 0.$$
 (17),

Card 2/3

The thermal conductivity of an...

S/170/63/006/002/011/018 B102/B186

$$T = -\frac{bh_0}{2\pi} \int_{-\infty}^{+\infty} \frac{\varphi_1(0,\beta)}{\varphi_2(0,\beta)} A(\beta) \cos\beta xd\beta \times$$

$$\times \int_{-l^{\infty}}^{0-1+l^{\infty}} [\Pi_{1}(u,\beta)(\lambda \sqrt{u^{2}-\beta^{2}b^{2}}\cos\sqrt{u^{2}-\beta^{2}b^{2}}\rho + \alpha b \sin\sqrt{u^{2}-\beta^{2}b^{2}}\rho) \times (21)$$

 $\times \exp(uv) du \left[u \varphi_1(u, \beta)\right]^{-1}$ 

is found. ho is the heat transfer coefficient for the interface between the heat giving medium and the wall while ho is that for the boundary surface between the wall and the heat absorbing medium.

ASSOCIATION: Sevastopol'skiy filial Odesskogo politekhnicheskogo instituta g. Sevastopol' (Sevastopol' Branch of the Odessa Polytechnic Institute Sevastopol')

SUBMITTED: April 9, 1962

Card 3/3

EWP(r)/EWT(1)/EPF(n)-2/BDS AFFTC/ASD/SSD

8/170/63/000/004/014/017

AUTHOR: Khrustalev, A. F.

TITLE: Nonstationary heat conduction problem for a cylinder

PERIODICAL: Inzhenerno-fizicheskiy zhurnal, v. 6, no. 4, 1963, 108-110

The author considers a nonstationary temperature field of an infinite solid cylinder under two different boundary conditions (r = R, z greater than 0; r = R, and z less than 0). In the theoretical discussion and equations, ho = the relative factor of heat between the heat-yielding medium and a cylinder; h = the relative factor of heat exchange between the cylinder and the heat-absorbing medium; R = the cylinder's radius; A(u) = an arbitrary function of the complex variable u; and To and omega are constants. The author derives an exact solution in closed form.

ASSOCIATION: Filial Odesskogo politekhnicheskogo instituta (Sevastopol) (Affiliate

of the Odessa Polytechnical Institute)

Jul 27, 62 SUEMITTED:

Card 1/1

### KHRUSTALEV, A.F.

Temperature field of a uniform half-space. Inzh.-fiz. zhur. 6 no.7: 126-127 J1 '63. (MIRA 16:9)

1. Filial Odesskogo politicheskogo instituta, Sevastopol<sup>1</sup>. (Temperature fields)

# KHRUSTALEV, A.F.

A contact problem in the theory of elasticity for bodies of limited size. Dokl. AN SSSR 151 no.5:1056-1059 Ag '63.

1. Sevastopol'skiy filial Odesskogo politekhnicheskogo instituta.
Predstavleno akademikom A.Yu.Ishlinskim.
(Boundary value problems) (Elasticity)

KHRUSTALEV, A. F. (Sevastopol')

"On the mixed problem of elasticity for bounded bodies"

report presented at the 2nd All-Union Congress on Theoretical and Applied Mechanics, Moscow, 29 January - 5 February 1964

ACCESSION NO: AP4018051

\$/0140/64/000/001/0139/0143

AUTHOR: Khrustalev, A. F.

TITLE: An axially symmetric mixed boundary value problem in the theory of elasticity for a transversely isotropic cylinder

SOURCE: IVUZ. Matematika, no. 1, 1964, 139-143

TOPIC TAGS: mixed boundary value problem, mixed problem, transversely isotropic cylinder, elasticity, elastic cylinder

ABSTRACT: A method is suggested for determining the stress in a bounded circular transversely-isotropic cylinder with the mixed boundary conditions

$$\sigma_r = -\frac{\partial}{\partial z} \left( \frac{\partial^2 \Phi}{\partial r^2} + \frac{b}{r} \frac{\partial \Phi}{\partial r} + a \frac{\partial^2 \Phi}{\partial z^2} \right) = 0 \quad \text{for } r = R; \ |z| > h,$$

$$\tau_{rz} = \frac{\partial}{\partial r} \left( \frac{\partial^2 \Phi}{\partial r^2} + \frac{1}{r} \frac{\partial \Phi}{\partial r} + a \frac{\partial^2 \Phi}{\partial z^2} \right) = 0 \quad \text{for } r = R; \ |z| < \infty,$$

$$u_r = r (a_{12}\sigma_r + a_{11}\sigma_\theta + a_{13}\sigma_z) = f(z) \quad \text{for } r = R; \ |z| < h,$$

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ACCESSION NO: AP4018051

where
$$a_{0} = -\frac{\partial}{\partial z} \left( b \frac{\partial^{2} \Phi}{\partial r^{2}} + \frac{1}{r} \frac{\partial \Phi}{\partial r} + a \frac{\partial^{2} \Phi}{\partial z^{2}} \right),$$

$$a_{z} = \frac{\partial}{\partial z} \left( c \frac{\partial^{2} \Phi}{\partial r^{2}} + \frac{c}{r} \frac{\partial \Phi}{\partial r} + a \frac{\partial^{2} \Phi}{\partial z^{1}} \right),$$

The problem involves the solution of the equation

$$\Delta_i^2 \Delta_i^2 \Phi(r; z) = 0$$

$$\left(\Delta_i^2 - \frac{\partial^2}{\partial r^2} + \frac{1}{r} \frac{\partial}{\partial r} + \frac{1}{S_i^2} \frac{\partial^2}{\partial z^2}, i = 1, 2\right)$$

subject to the above conditions where the terminology is that of S. G. Lekhnitskiy (Teoriya uprugosti anizotrophogo tela, GITTL, M.-L., 1950). A general solution of the differential equation is given. In order to satisfy the boundary conditions, certain unknown functions must be determined. This leads to a pair of integral equations. By using the results of N.N. Lebedev and Ya. S. Uflyand (Osesimmetrichnaya kontaktnaya zadacha dlya uprugogo sloya, PMM, t. 22, vy\*p. 3, 1958), the problem is reduced to finding the solution  $\varphi(t)$  of a Fredholm integral equation of the second kind. The following formula involving  $\varphi(t)$  is then obtained

Card 2/3

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Card 3/3		•							

KHRUSTALEV, A.F. (Sevastopol')

A mixed problem in the theory of elasticity for a plane parallel layer.

In2h.2hur. 4 no.31553-556 '64.

(MIRA 17:10)

KHRUSTALEV, A.F.

Steady-state problem in the heat conduction theory for a plane-parallel layer. Inzh.-fiz. zhur. 7 no.8:47-50 Ag '64. (MIRA 17:10)

1. Filial Odesskogo politekhnicheskogo instituta, Sevastopol'.

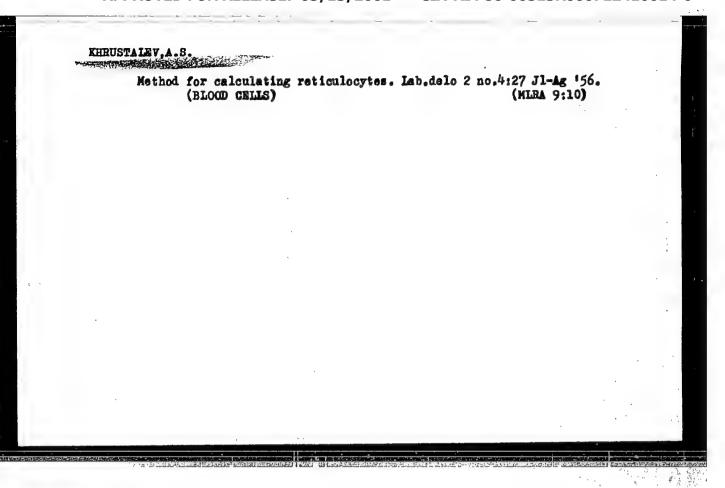
Contact problem of thermoelasticity for a semispace. Inzh.zhur. 5 no.14180-183 165. (MIRA 18:4

RYZHIKOV, A.S., kandidat meditsinskikh nauk; KHRUSTALEV, A.N., doktor meditsinskikh nauk, zavednyushchiy; KALASHNIKOVA, R.R., glavnyy vrach.

Treatment of patients with enlarged veins of the lower extremities. Sov. med. 17 no.6:33-34 Je '53. (MLRA 6:6)

1. Khirurgicheskoye otdeleniye Kolpinskoy bol'nitsy Leningrada (for Ryshikov and Khrustalev). 2. Kolpinskaya bol'nitsa Leningrada (for Kalashnikova).

(Veins--Diseases)



BARUSTALLY A-V.

AUTHORS:

Margulis, U.Ya., Khrustalev, A.V.

89-10-17/36

TITLE:

Computation and Measuring of the Y-Field of a Plane Source (Raschet 1 immercity - polya ot ploskogo istochnika)

PERIODICAL:

Atomnaya Energiya, 1957, Vol. 3, Nr 10, pp. 338-341 (USSR)

ABSTRACT:

The equations for the calculation of the dose of a plane source are derived theoretically and herefrom the isodose curves are formed. Further, measuring of the dose on a quasi-plane source (11 adjoining, active rods of a length of 1 m) are described with 418 mC. As the quintessence of all delibeations it is shown that an apparatus with a source consisting of 2 parallel plates with a distance of 25,44 cm and a total activity of Q = 1000 milligram - radium equivalent possesses an efficiency of 35,616 kg, where in the center of both plates there is a dose of 0,21 r/min. If, however, an apparatus is used for which an equivalent, cylindrical source of equal strength is used (25,44 cm, length 100 cm), then only an efficiency of 16,18 kg exists, where,

however, in the center of the source, there is a dose of 0,291 r/min. There are 7 figures.

SUBMITTED:

October 26, 1956

AVAILABLE:

Library of Congress

Card 1/1

Dissertation: "Investigation of Heat Exchange by Madiation in a high Efficiency Boiler-Furnace." Cand Tech Sci, Power Engineering Inst iment G. M. Krzhizhanovskiy, Acad Sci USSK, 20 May 54. Vechernyaya Moskwa, Moscow, 11 May 54.

S0: JUN 284, 26 Nov 1954

#### CIA-RDP86-00513R000722410014-0 "APPROVED FOR RELEASE: 03/13/2001

KHRUSTALEV. B.A. -

AID P - 2392

: USSR/Engineering Subject

Pub. 110-a - 6/15 Card 1/1

Filimonov, S. S., Khrustalev, B. A. and Kolchenogova, I.P., Authors

Kand. Tech. Sci.

: Research on heat transfer in boiler furnaces Title

Periodical: Teploenergetika, 7, 30-33, J1 1955

: Tests made on heat transfer in specially-built furnaces Abstract

are described. A comparison is made with standard

equipment. According to the results reported, convective heat transfer is desirable for furnaces of small dimensions. The standard design of the boiler unit appears to be unsatisfactory for some types of furnaces. Four diagrams. Seven Russian references, 1949-1954.

Institution: Power Institute of the Academy of Science, USSR

Submitted : No date

KONAKOV, P.K., doktor tekhnicheskikh nauk; FILIMONOV, S.S., kandidat tekhnicheskikh nauk; HHRUETALEY, B.A., kandidat tekhnicheskikh nauk.

Calculation of heat exonange in boiler furnaces [with summery in English]. Teploenergetika 4 no.8:49-53 Ag '57. (MERA 10:9)

1. Bnorgeticheskiy institut Akademii nauk SSSR. (Boilers) (Heat--Transmission)

KHRUSTALEV, IA.

AUTHOR:

KONAKOV, P.K., FILIMONOV, S.S., KHRUSTALEV, B.A. PA - 3562 On the Calculation of Radiative Heat Exchange in a Cooled Combustion Chamber. (K rashetu luchistogo teploobmena v okhlazhdayemykh kame-

rakh goreniya, Russian)

PERIODICAL:

Zhurnal Tekhn. Fiz., 1957, Vol 27, Nr 5, pp 1066 - 1075 (U.S.S.R.)

ABSTRACT:

A scheme for the heat exchange process in combustion chambers is suggested, which makes it possible to determine the required radiation temperature T<sub>S</sub> and to calculate the radiation heat exchange. It is assumed that hear the heat absorbing surfaces there is a layer of the medium which is in equilibrium with radiation, the molecular temperature of the medium and the radiation temperature being equal to each other. It is assumed that on the way from the balanced layer to the wall radiation is not in interaction with the medium, i.e. there is a transfer of radiation energy by effusion. It is therefore assumed that the temperature of this layer is equal to the T<sub>S</sub> on the heat-absorbing surface. The temperature of the balanced layer adjusts itself in accordance with an interaction between the medium and the radiation in the core of the flow.

The molecular-kinetic temperature of the balanced layer is determined by means of a field analysis of the molecular temperatures of the ignition chamber. Thus, the balanced layer dicides the ignition chamber into two zones: one that is close against the

Card 1/2

PA - 3562

On the Calculation of Radiative Heat Exchange in a Cooled Combustion  $C_{\text{hamber}}$ .

wall and comprises the domain from the heat absorbing surface to the balanced layer. The second zone, the medium core, comprises the rest of the space. The existence of a radiation equilibrium near the heat absorbing surfaces is proved theoretically and experimentally. The thickness of the balanced layer is measured in millimeters. On the basis of what has been said it is possible to determine the radiation temperature on the heat-absorbing surface and to calculate the radiative heat exchange in the combustion chamber. (With 10 illustrations and \$ Spavic references)

ASSOCIATION:

Institute for Energetics "G.M.KRZHIZHANOVSKIY", Moscow

PRESENTED BY:

SUBMITTED:

17.7.1956

AVAILABLE:

Library of Congress

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	lue	(Heat Fower Engineering, Mr 1) Nescow, lay p. Errata slip inserted. No. of copies	printed not given.  of Fablishing House, V. A. Kotov; Tech, Ed.; Yu. V. Bylins;  of Fablishing House, V. A. Bauis, Doctor of Technical Schemes.  Frograms (Resp. Ed.); G. T. Rollodovskiy, Doctor of Technical  Frograms (Resp. Ed.); G. T. Rollodovskiy, Botor of Technical  Frograms E. I. Yushicheritovs, Canaldate of Technical Schemes; (Sorretary);  Z. L. Winnersty, Canaldate of Technical Schemes (Sorretary);  Z. G. Programson, Earling Canaldate of Technical Schemes.	t is intended for scientists and engineers working steam bollers.	TRACE: This is a collection of 9 articles on the circulation water and seter-empty mixture in boliers, bubbling processes, palastion of pressure; temperature fields in combustion chambers, palastion of pressure; temperature fields in combustion of a redission and the collection of a radiation and temperature from the collection of manifest problems of minimum processes occuring in the stemperature of a	political destrictions. References appearance monthly and article.  Soft article at the reductive lettic laboratories in cooperation are conflicted at the reductive laboratories. No. 9.	The result of the control of the con	tester in a converse.  The service of the distribution of volume vapor content and all content along the alevation of the bubbling volume and air content along the action of the bubbling volume. Itself the bublic water reduct vector for any service and a terminate reducted of the performed seems under water and characteristics of the performed presents and characteristics of the performed presents and characteristics of the performed presents are along the decrease of vapor content. An increase presents in a decrease of vapor content. An increase the yolune vapor content.	Paleations of Pressure in the Flow of Cas-Liquid.	The metale describes experiments in pressure 7th 7th 7th four 1th a long pipes of different dismocra-25d, 47th 7th four 1th and pressure 2th a long pipes and of the four 1th and pressure 1th an	and you contain changed from 0.05 to 0.99. Uraphirate the grace of experimental results are given. Investigation of assembly Z. L., and R. L. Simeyerove. Investigation of assembly Z. L., and R. L. Simeyerove. Investigation	wor Vapor Mater Marters in the of the factor of the state article the authors describe problems in determining the average values of steam volume contents of articles of steam volume contents of papers and in contains of rectangular or and in contains of rectangular value of graphs are given.	Temperature Fields in	brastion Chastors in the control of	chappler, D. H. Steam Bolton of a Solar Heat Energy Station	The author presents date on the performance of stems bollers operating on solar heat energy. Geberal diagrams of a boller and tables of principal characteristic are given.	Surimor, Mu. A. Investigation of Radistion Meat Transfer in Seriess of Gray Bodies	The author develops a theory of radiation and radiation heat transfer. The equations appearing in this article becarected, probability interpretation. The article is di- vided into two parter 1) Solution of a sized problem on radia- ation heat archange in a system of gray bodies in a distinction action, and 2) Solution of a mixed problem of radiation heat
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Temperature field in combustion chambers. Teploenergetika [Energ. inst.]
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KONAKOV, Petr Kuz'mich, prof., doktor tekhn.nauk; FILIMONOV, Sergey Sergeyevich, kand.tekhn.nauk; KHRUSTALEV, Boris Aleksandrovich, kand.tekhn.nauk; ARNOL'D, L.V., prof., retsenzent; LAKHANIN, V.V., prof., doktor tekhn.nauk, nauchnyy red.; SHLEHNIKOVA, Z.V., red.izd-va; BODROVA, V.A., tekhn.red.

[Heat exchange in the combustion chambers of steam boilers]
Teploobmen v kamerakh sgoraniis parovykh kotlov. Moskva, Izd-vo
"Rechnoi transport," 1960. 269 p. (MIRA 13:5)
(Boilers) (Furnaces)

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Filimonov, S. S., Khrustalev, B. A., Adrianov, V. N.

AUTHORS:

TTLE:

On the Theoretical Principles of the Method of the Two

Radiometers 19

PERIODICAL:

Zhurnal tekhnicheskoy fiziki, 1960, Vol. 30, No. 6,

pp. 690-698

TEXT: V. S. Kocho (Ref. 1) introduced a method for the separate measurement of the radiation flow and the convective flow (method of two radiometers). This was used in the investigation of the heat exchange in the Siemens-Martin furnaces (Ref. 1) and in the combustion chambers (Refs. 2, 3). In the present paper this method is analyzed. The heat absorption at the relevant place of heating is measured simultaneously by means of two radiometers with different degrees of blackening A<sub>1</sub>, A<sub>2</sub>, of the heat-absorbing elements. The formulas (1) and (2) are written down for the calculation of the heating flow. It is assumed that the density E<sub>incident</sub> of the incident radiation is equal for both radiometers. Furthermore, it is assumed that

Card 1/3

On the Theoretical Principles of the Method S/057/60/030/06/15/023

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of the Two Radiometers

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the convective flows for both radiometers are equal and = q<sub>k</sub>. Formula (5) is derived for E<sub>incident</sub> and (6) for q<sub>k</sub> which are commonly used in calculations. The constancy of E<sub>incident</sub> is maintained if the measuring surface of the radiometer is considerably smaller than the over-all surface of the heat exchanger. In order to prove the accuracy of the assumption of the mutual independence of the convective and the radiation current the experimental investigation described herein was carried out. This was done by means of 3 radiometers. This proof was based on the idea that, if the assumption was right, any pair of radiometers would yield the same results as the other two pairs. The investigation showed that the hypothesis of the mutual independence of the radiation flow and the convective flow in the medium boundary layer in the combustion chambers is in practice maintained with sufficient accuracy. The experiments have shown that by the method of two radiometers and by fulfilling the conditions

 $\frac{A_2}{A_1}$  < 0.2 and  $\frac{F_{radiometer}}{F_{heating-}}$  < 1 satisfactory results were obtained.

Card 2/3

On the Theoretical Principles of the Method S/057/60/030/06/15/023 81594 B012/B064

This should also be considered in the production of the radiometers. In the present paper also a mathematical analysis of the accuracy of formulas (5) and (6) was carried out on the basis of the error theory. The two methods applicable in this case are given. On the basis of this analysis formulas (10), (11), (12), and (13) were derived. With these formulas all the extreme relative errors in the required quantities can be calculated in dependence of all the factors influencing such quantities. The analysis showed that the errors of and  $\delta_{\mathbf{q_k}}$  diminish with decreasing ratio incident

This was confirmed by the results obtained from the experimental investigation. There are 8 figures and 4 Soviet references.

SUBMITTED: November 18, 1957

Card 3/3

# KHRUSTALEV, B. A., and FILIMONOV, S. S.

"Evaluation of Local Heat Transfer and Hydraulic Resistance at Turbulent Flow of Water in Tubes with Different Inlets."

Report submitted for the Conference on Heat and Mass Transfer, Minsk, BSSR, June 1961.

S/124/61/000/011/027/046 D237/D305

AUTHORS: Filimonov, S.S., Khrustalev, B.A., and Adrianov, V.N.

TITLE: Measuring convective and radiant components of a complex heat transfer by two radiometers

PERIODICAL: Referativnyy zhurnal, Mekhanika, no. 11, 1961, 95, abstract 11B630 (Sb. Konvektiv, i luchistyy teploobmen, M., AN SSSR, 1960, 133 - 144)

TEXT: The method of separate measurements of radiant and convective streams proposed by V.S. Kocho (Stal', 1950, No. 3) depends on simultaneous measurement of heat intensity on the given point of the surface by two radiometers, whose heat absorbing elements have different coefficients of absorption, assuming radiant and convective streams on the surface of the meters, are independent of each other. The results are given of an experimental check (by means of three radiometers) of applicability of the method in various combustion chambers. [Abstractor's note: Complete translation].

Card 1/1

32381 S/124/61/000/012/025/038 D237/D304

26.5200

AUTHORS:

Filimonov, S. S., and Khrustalev, B. A.

TITLE:

On calculating heat transfer and hydraulic drag in the laminar flow of fluid in tubes

PERIODICAL:

Referativnyy zhurnal, Mekhanika, no. 12, 1961, 95, abstract 12B655 (V sb. Konvektivn. i luchistyy teploobmen. M., AN SSSR, 1960, 221-

232)

TEXT: The method of processing experimental data is given, allowing the calculations of local and mean characteristics of heat transfer and hydraulic resistance in laminar flow of fluids in tubes heated in a constant flow of heat under the condition of simultaneous development of thermal and hydrodynamic boundary layers. It is shown that the dependence of the Nusselt No. on Gretz criterion,

Card 1/4

(1)

32381 On calculating heat... S/124/61/000/012/025/038 D237/D304

$$\begin{pmatrix}
N_{fx} = f (Gz^{\dagger}) \\
N = \frac{qd}{(t_{wx} - t_{fx}) h_{fx}}, Gz^{\dagger} = \frac{x/d}{P^{\dagger}f}
\end{pmatrix},$$

does not fully reflect the influence of all parameters on the mode of development, as the spread over the layer of experimental points depends on the magnitude of thermal flow q on the temperature of the fluid on entering the experimental region. The author succeeded in representing the experimental data by

$$N_{fx} \left( \frac{P_{wx}}{P_{fx}} \right)^{1/3} = 4.36 + 0.36 x^{-1/2} \times 10^{-18X}$$
, (2)

Card 2/4

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On calculating heat...

which enables the calculation of the wall temperature at any point of the tube under the condition of constant thermal flow with simultaneous formation of thermal and hydrodynamic boundary layers. Graphs of  $N_{fx} (P_{wx} / P_{fx})^{1/3}$ v. X are given for the experimental data of various authors. A formula is proposed for the determination of the region of thermal stability, and a graph is given of the mean Nusselt No. N v. mean value of the criterium X. Experimental data on hydraulic resistance for the front part of the tube  $((x/d) R_f^{-1}, 0.065)$ factorily described by

$$\frac{\zeta_{x}^{R_{f}^{i}}}{(P_{wx}/P_{fx})^{1/3}} = 64 + 3.2 \left(\frac{x/d}{R_{f}^{i}}\right)^{-0.56} 10^{-14.6} \frac{x/d}{R_{f}^{i}}$$
(3)

Card 3/4

ACCESSION NR: AP4000397

S/0294/63/001/001/0017/0023

AUTHORS: Khrustalev, B. A.; Kolchenogova, I. P.; Rakov, A. M.

TITLE: Spectral radiation coefficients for tantalum, molybdenum and niobium

SOURCE: Teplofizika vy\*sokikh temperatur, v. 1, no. 1, 1963, 17-23

TOPIC TAGS: temperature measurement, optical pyrometry, tantalum, molybdenum, niobium, radiation, radiative heat transfer, high temperature, radiation coefficient, radiation spectrum

ABSTRACT: The purpose of the investigation was to determine, for purposes of optical pyrometry, the emission coefficients of the materials, which were determined for the effective wavelength 0.65 micron corresponding to the spectral region accommodated by the KS-filter and the human eye. The radiation coefficients were determined over a wide range of temperatures for different surface conditions of the investigated material. The average measurement accuracy was 14.6% near 1000C and 5% near 2000C. The mean square deviation

Card 1/2.

ACCESSION NR: AP4000397

of the experimental points from their averaging curves was 3.2, 6.2, and 6.1% for tantalum, molybdenum, and niobium, respectively, and is in good coordination with the maximum relative error. The orig. art. has: 4 figures and 2 tables.

ASSOCIATION: Energeticheskiy institut im. G. M. Krzhizhanovskogo (Power Engineering Institute)

SUBMITTED: 17May63

DATE ACQ: 13Dec63

ENCL: 01

SUB CODE: AS

NO REF SOV: 004

OTHER: 010

Card 2/3

KHRUSTALEV, B. A.; RAKOV, A. M.; DMITRIYEV, A. A.; KOLCHENOGOVA, T. P.

"Investigation of radiation coefficients of heat-resistant materials."

report submitted for 2nd All-Union Conf on Heat & Mass Transfer, Minsk,

G. M. Krzhizhanovskiy Power Inst.

4-12 May 1964.

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	AUTHOR: Adrianov, V. N.; Khrustalev, B. A.; Kolchenogova, I. P. 54	
	ORG: none	
	TITLE: Radiative-convective heat transfer of a high temperature flow of gas in a channel	
	SOURCE: Moscow. Energeticheskiy institut. Teploobmen v elementakh energeticheskikh ustanovok (Heat exchange in power installation units). Moscow, Izd-vo Nauka, 1966, 134-150	
	TOPIC TAGS: radiative heat transfer, convective heat transfer, gas flow	
	ABSTRACT: The article is devoted to a combined theoretical and experimental treatment of the problem of complex heat transfer between a high temperature gas flow and the cold surface of a channel. The theoretical analysis arrives at a method for determining the quantities which enter into the dimensionless relationship describing the process. For the experimental investigation, a special apparatus was built to study radiative-convective heat transfer during the movement of the products of the combustion of a gaseous fuel in cylindrical channels. The article gives a diagram of the experimental apparatus. Four series of experiments were carried out in channels of different diameters. The experimental results are exhibited in extended tables. On	
	Card 1/2	
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ne basis of the experime	ental data, the following rel	ationship was arrived at:	
	$-A\varphi [1+(1-\varphi)^{0,1}(16,3Re^{0,10}_{\omega}-70)]$		
ere $\theta$ is the dimension is the radiation cri	less temperature of the gases terion. Orig. art. has: 24	$s$ ; $\psi$ is a temperature simple formulas, 5 figures and 2	tables.
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RELINSKAYA, A.V.; BOCUSLAVSKAYA, S.A.; DUBIN, A.S.; PRUSSAK, O.V.; STARTSEV, V.I.; DAVIDOVICH, Ya.I., doktor yurid.nauk, red.; KHRUSTALEV, B.P., red.; SHILOV, L.A., red.; VODOLAGINA, S.D., tekhn.red.

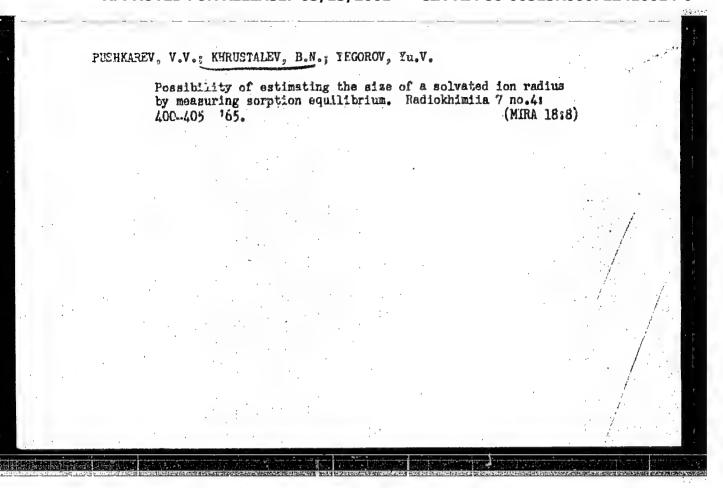
[Socialist competition in Leningrad enterprises during the years of the first five-year plan, 1928-1932] Sotsialisticheskos sorevnovanie na predpriiatiiakh Leningrada v gody pervoi piatiletki, 1928-1932 gg.; sbornik dokumentov i materialov. Pod red. IA.I.Davidovicha. Leningrad, Izd-vo Lening.univ., 1961. 343 p. (KIRA 14:4)

l. Leningrad. Gosudarstvennyy arkhiv Oktyabr'skoy revolyutsii i sotsialisticheskogo stroitel'stva.

(Leningrad--Socialist competition)

YEGGROV, Iu.V.; LYHBIMDV, A.S.; KHRUSTALEV, B.V.

Radiocolloids in sorption systems. Part 3: Effect of hydrogenion concentration. Radiokhimiia 7 no.4:386-394 165. (MIRA 18:8)



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SOURCE CODE: UR/0363/66/002/007/1200/1205

AUTHOR: Kharakhorin, F. F.; Aksenov, V. V.; Gambarova, D. A.; Khrustalev, B. P.; Kul'bich, R. K.

ORG: none

TITIE: On the mechanism of change of the conduction sign during heat treatment of n-InSb/Paper presented at the All-Union Conference on Diffusion in Semiconductors held in Leningrad on 2 December 1904/

SOURCE: AN SSSR. Izv. Neorg materialy, v. 2, no. 7, 1966, 1200-1205

TOPIC TAGS: indium compound, antimonide, semiconductor conductivity

ABSTRACT: An attempt was made to identify the impurities in InSb on the basis of their characteristic emissions and half-lives following heat treatment of InSb in quartz ampoules activated by a flux of slow neutrons (0.9-2.4 x 10<sup>13</sup> n/cm² sec) in an atomic pilo. It was shown by the gamma-spectroscopic mothod that the radioactive impurities Na²4, Cu²4 and Si³1 migrated from the neutron-activated quartz into n-InSb. The experimental data indicate that the chief cause of the change of the conduction sign during heat treatment of n-InSb is the diffusion of copper. It was shown that vacuum annealing of the ampoules prior to the activation decreases the activity of the N-InSb samples by a factor of 20 to 60. Authors thank L. A. Bovina, M. F. Poluboyarinova and V. G. Vinogradova for their assistance. Orig. art. has: 6 figures and 2 tables.

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Card 1/1 nat .UDC: 546.682'861:537.31133

ZYRIN, G., inzh.; YEFIMENKOV, R., inzh.; KHRUSTALEV, G., inzh.
"IUnost" television receiver. Radio no.1:21-25 Ja '66.
(MIRA 19:1)

SOV/105-58-7-12/32

AUTHOR: Khrustalev, I. K., Candidate of Technical Sciences

TITLE: New Wiring Diagrams for Starting- and Regulating Rheostats of Asynchronous Motors (Novyye skhemy soyedineniya pusko-

regulirovochnykh soprotivleniy asinkhronnykh dvigateley)

PERIODICAL: Elektrichestvo, 1958, Nr 7, pp. 55 - 56 (USSR)

ABSTRACT: At present a method of connecting the relays of magnetic

rotor stations with which a successive disconnecting and connecting of the resistance-steps in the motor-rotor-circuit takes place, is used in circuits of the relays contactor equipment of asynchronous motors. - The relatively small number of operational stages of the resistance leads to a deterioration of the starting- and retarding properties of the motor and to a decrease of uniformity when regulating

their velocity, as well as to the formation of inadmissible dynamic overloads. These faults can be removed by parallel-

or parallel-series connection of the contactors of the magnetic rotor stations. A 6-step rheostat of metal was cal-

Card 1/2 culated and completed in the Coal Field of Karaganda. A great

SOV/105-58-7-12/32

New Wiring Diagrams for Starting- and Regulating Rheostats of Asynchronous Motors

number of mechanical rheostat-characteristics of the motor can be obtained by means of such metal rheostats which are connected according to the wiring diagram given here. The safety of motor-control can in this manner be increased.

There are 3 figures and 1 table.

ASSOCIATION: Sibirskiy metallurgicheskiy institut

(Siberia Institute of Metallurgy)

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1. Variables resistors--Wiring diagrams 2. Induction motors

--Design

Card 2/2